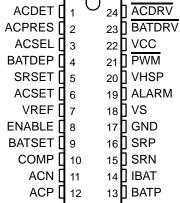
b 24700, b 24701 NOTEBOOK PC BATTERY CHARGE CONTROLLER AND SELECTOR WITH DPM

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- Dynamic Power Management, DPM Minimizes Battery Charge Time
- Integrated Selector Supports Battery Conditioning and Smart Battery Learn Cycle
- Selector Feedback Circuit Insures Break-Before-Make Transition
- ±0.4% Charge Voltage Accuracy, Suitable for Charging Li-lon Cells
- ±4% Charge Current Accuracy
- 300-kHz Integrated PWM Controller for High-Efficiency Buck Regulation
- Depleted Battery Detection and Indication to Protect Battery From Over Discharge
- 15-μA Sleep Mode Current for Low Battery Drain
- Designed for Charge Management of NiCd/NiMH and Li-Ion/Li-Pol Battery Packs
- 24-Pin TSSOP Package

application schematic

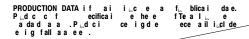
PW PACKAGE (TOP VIEW)



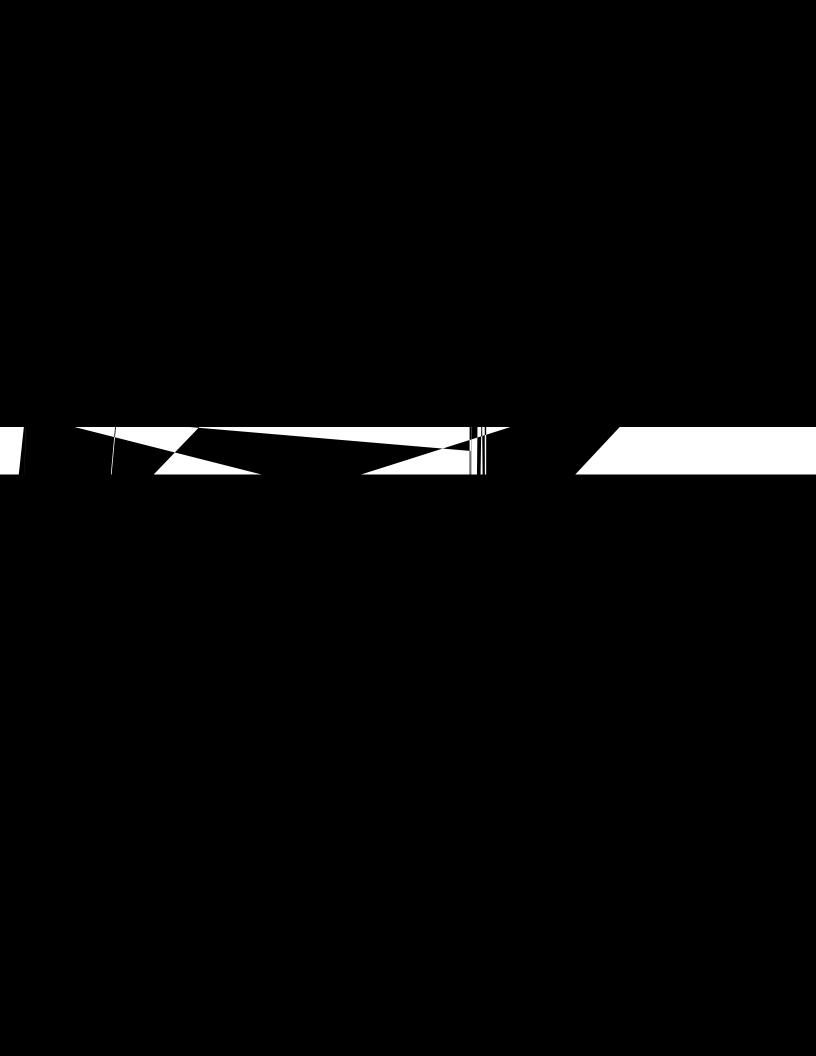
D1 R5 ADAPTER MBRD640CT 0.025 SUPPLY DPAK 1 W	Q2 IRFR5305	33µН D05022p–333		
—	αſ	Q1 IRFR5305 (***)	Q3 VBAT IRFR5305	TO SYSTEM
100Ω - 111 ACN	ACDRV 24 = 30	I I R6	14	D4 17 V 3891 399.175 IT366.067 (7.65 367.S7.46 31.65 63 391
1 μF 12 ACP	VCC 22 4.7 Ω	*	C5, C6 — 22μF x2	$ \begin{array}{c c} & D4 \\ 17 \text{ V} & \stackrel{R14}{>} 523 \text{ k} \Omega & \stackrel{=}{=} \end{array} $
1 ACDET	PWM 21	J =	12.6 V + 35 \/	
\$ 100 kΩ	$ \begin{array}{c c} & 4.7 \mu F \\ \hline & 8RP & 16 \end{array} $	R10 20Ω 	R9 57.6 kΩ	R15 ≥57.6 kΩ
3 ACSEL	SRN 15	C3 10μE 10Ω	<u> </u>	=
19 ALARM	BATP 13 B330	Β330 100 κΩ	9	
	BATDRV 23	J1 100 102	=	
ACSET	VS 18			
ACPRES	VHSP 20	18	V 	→ VCC
20 kΩ 5VREF	BATSET 9			
C7 VREF	BATDEP 4	04	499 kΩ	VBAT
3.3 _µ F C8 150 pF 10 COMP	GND 17	— C4 10μF 35 V	180 pF ≥ 76.8 kΩ	
C9 R13	J +	<u>+</u> +	<u>+</u> +	
CHARGE VOLTAGE SETPOINT				UDG-00138

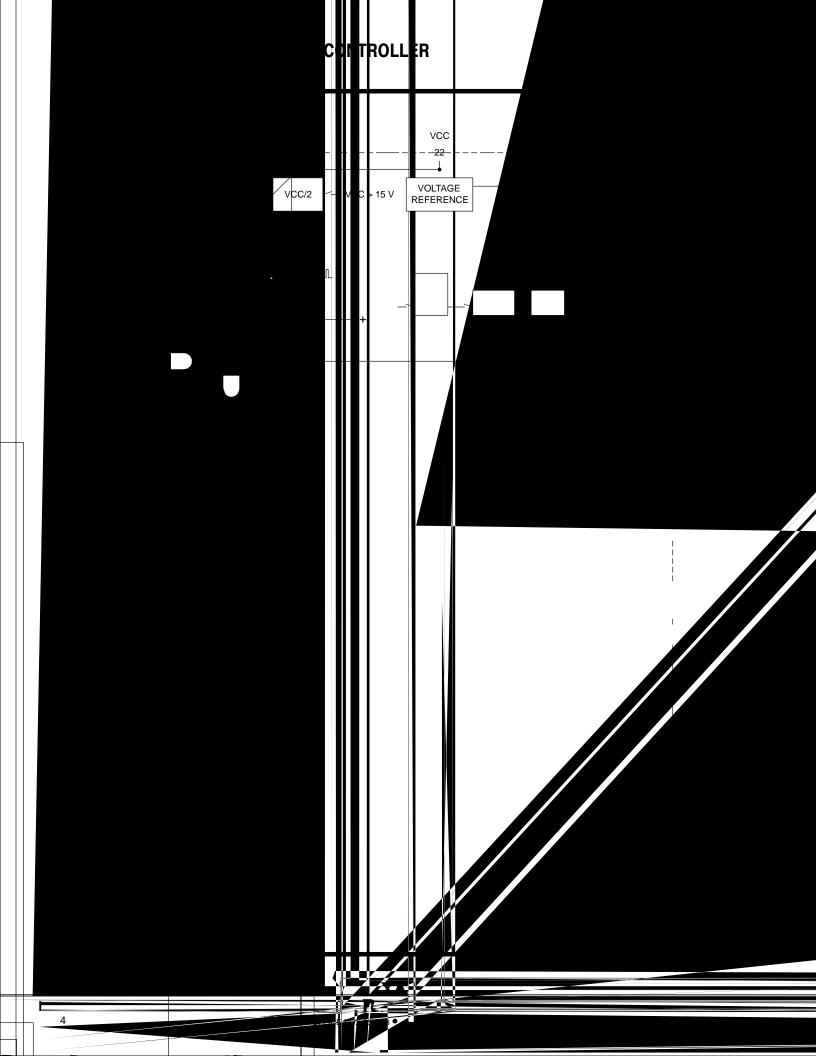


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electrical characteristics ($T_A = T_{OPR}$, 7.0 Vdc V_{CC} 20.0 Vdc, all voltages relative to V_{SS}) (unless otherwise specified) (continued)

adapter current-sense amplifier

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
9 _m	Transconductance gain		90	150	210	mA/V
CMRR	Common-mode rejection ratio	See Note 1		90		dB
VICR	Common-mode input voltage range (ACP)		7.0		V _{CC} +0.2	V
ISINK	Sink current (COMP)	COMP = 1 V, (ACP – ACN) = 10 mV	0.5	1.5	2.5	mA
I _{IB}	Input bias current (ACP, ACN)	ACP = ACN = 20 V, SRSET = 0 V, VCC = 20 V, ACSET = 1.25 V	15	25	35	μΑ
	Input bias current accuracy ratio (ACP, ACN)	ACP = ACN = 20 V, VCC = 20 V, ACSET = 1.25 V	0.95	1.00	1.05	
VSET	AC current programming voltage (ACSET)		0		2.5	V
A _V	AC current set gain	$0.65~V \le ACSET \le 2.5~V,~12~V \le ACP \le 20~V,$ $-40^{\circ}C \le T_{A} \le 85^{\circ}C,~See~Note~4$	24.5	25.5	26.5	V/V
	Total ac current-sense mid-scale	ACSET = 1.25 V, $T_A = 25$ °C, See Note 5	-5%		5%	
	accuracy	ACSET = 1.25 V, -40° C \leq T _A \leq 85°C, See Note 5	-6%		6%	
	Total ac current-sense full-scale	ACSET = 2.5 V, T _A = 25°C, See Note 5	-3.5%		3.5%	
	accuracy	ACSET = 2.5 V, -40° C \leq T _A \leq 85°C, See Note 5	-4%		4%	

battery voltage error amplifier

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
9m	Transconductance gain		75	135	195	mA/V
CMRR	Common-mode rejection ratio	See Note 1		90		dB
VICR	BATSET common-mode input voltage range		1		2.5	V
V_{IT}	Internal reference override input threshold voltage		0.20	0.25	0.30	V
ISINK	Sink current COMP	COMP = 1 V, (BATP – BATSET) = 10 mV, BATSET = 1.25 V	0.5	1.5	2.5	mA
		$T_A = 25^{\circ}C$	1.241	1.246	1.251	
V_{FB}	Error-amplifier precision reference voltage	$0^{\circ}C \leq T_{A} \leq 70^{\circ}C$	1.239	1.246	1.252	V
		$-40^{\circ}\text{C} \le \text{T}_{A} \le 85^{\circ}\text{C}$	1.234	1.246	1.254	

NOTES: 1. Ensured by design. Not production tested.

2. $I_{BAT} = \frac{SRSET}{R_{SENSE}} \times \frac{1}{A_{V}}$ 3. Total battery-current set is based on the measured value of (SRP–SRN) =

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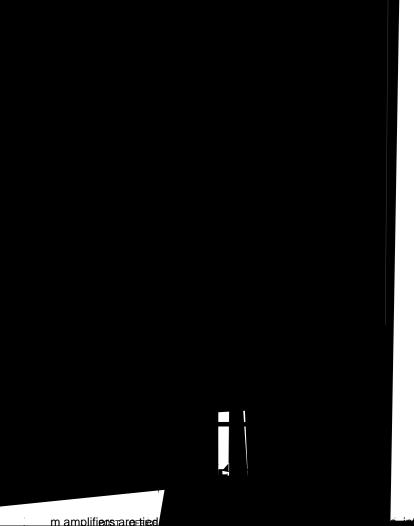
electrical characteristics ($T_A = T_{OPR}$, 7.0 Vdc V_{CC} 20.0 Vdc, all voltages relative to V_{SS}) (unless otherwise specified) (continued)

MOSFET gate drive

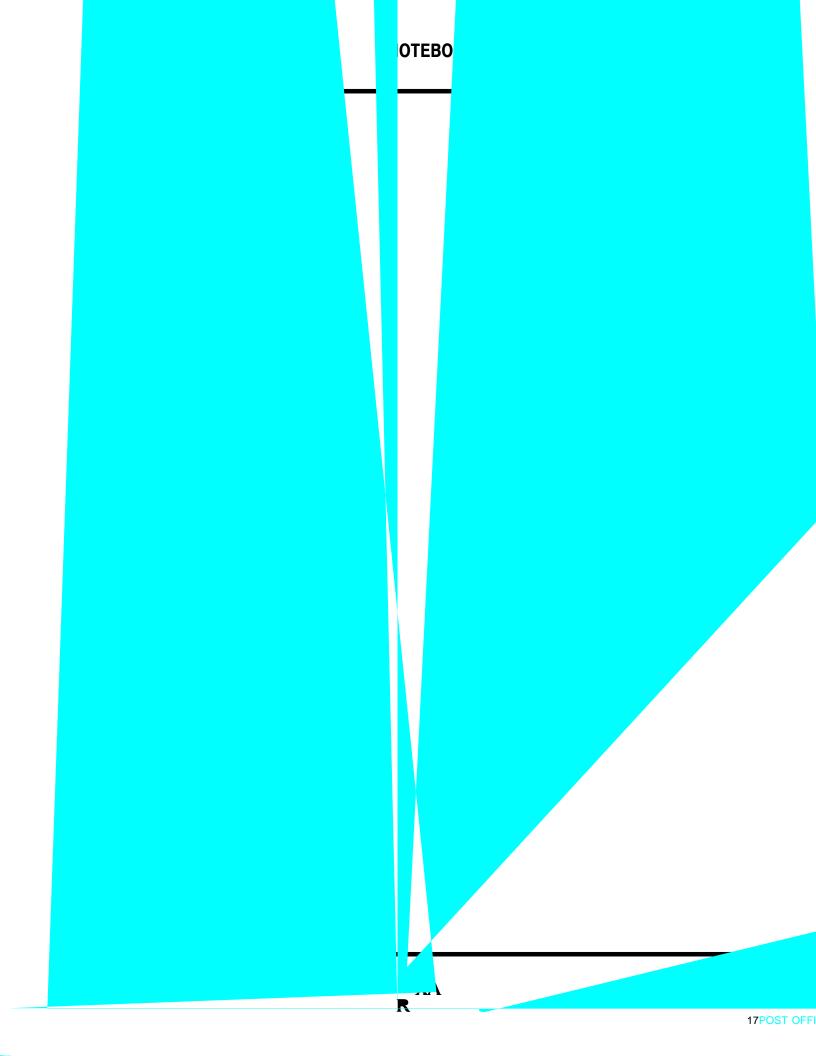
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
	AC driver R _{DS(on)} high	V _{CC} = 18 V		150	250	Ω
	AC driver R _{DS(on)} low	V _{CC} = 18 V		60	120	Ω
	Battery driver R _{DS(on)} high	V _{CC} = 18 V		200	370	Ω
	Battery driver R _{DS(on)} low	V _{CC} = 18 V		100	170	Ω
t _{Da}	Time delay from ac driver off to battery driver on	ACSEL 2.4 V		0.5	1.5	μs
t _{Db}	Time delay from battery driver off to ac driver on	ACSEL 0.2 V ↑ 2.4 V		1.0	2.0	μs
.,	DIA/AA daisaa kiah lasal astasta dibara	$I_{OUT} = -10 \text{ mA}, \text{ VCC} = 18 \text{ V}$	-0.12	-0.07		\ /
VOH	PWM driver high-level output voltage	I _{OUT} = -100 mA, VCC = 18 V	-1.2	-0.7		

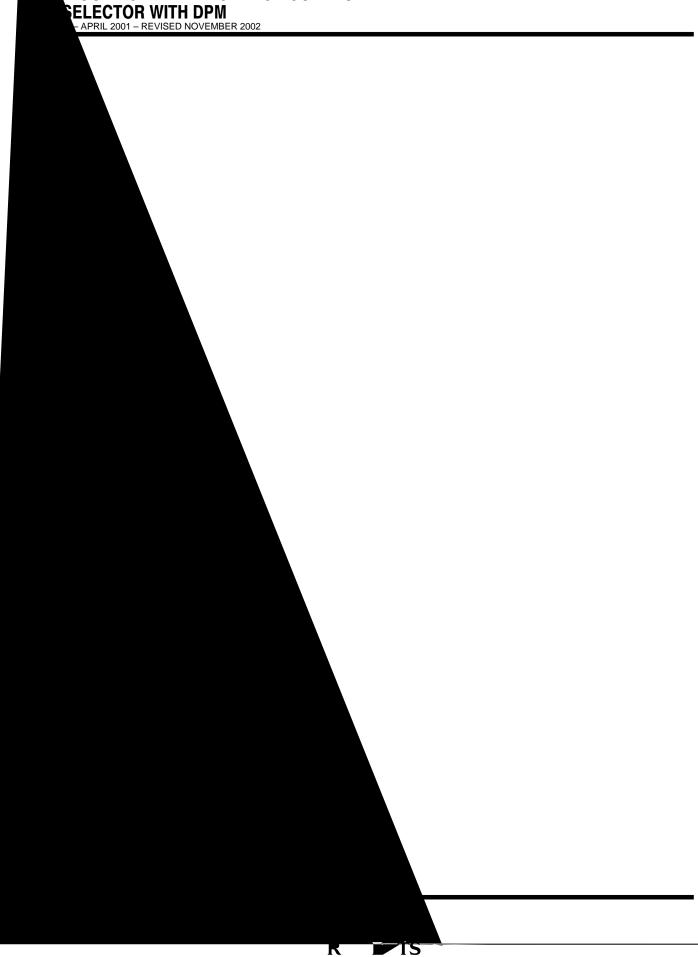


NOTEBOOK PC BATTERY CHARGE CONTROLLER AND SELECTOR WITH DPM SLUS452B - APRIL 2001 - REVISED NOVEMBER 2002 RXA 13P



700, b 24701 EBOOK PC BATTERY CHARGE CON1 SELECTOR WITH DPM 52B – APRIL 2001 – REVISED NOVEMBER 2002





APPLICATION INFORMATION

Rs

UDG-00117



APPLICATION INFORMATION

The RMS current through the MOSFET is defined as:

$$I_{IN}(RMS) = I_{IN}(avg) \times \sqrt{\frac{1}{D}} A_{RMS}$$

Schottky rectifier (freewheeling)

The freewheeling Schottky rectifier must also be selected to withstand the input voltage, V_{IN}. The average current can be approximated from:

$$I_{D1}(avg) = I_{O} \times (1 - D) A$$

choosing an inductance

Low inductance values result in a steep current ramp or slope. Steeper current slopes result in the converter operating in the discontinuous mode at a higher power level. Steeper current slopes also result in higher output ripple current, which may require a higher number, or more expensive capacitors to filter the higher ripple current.

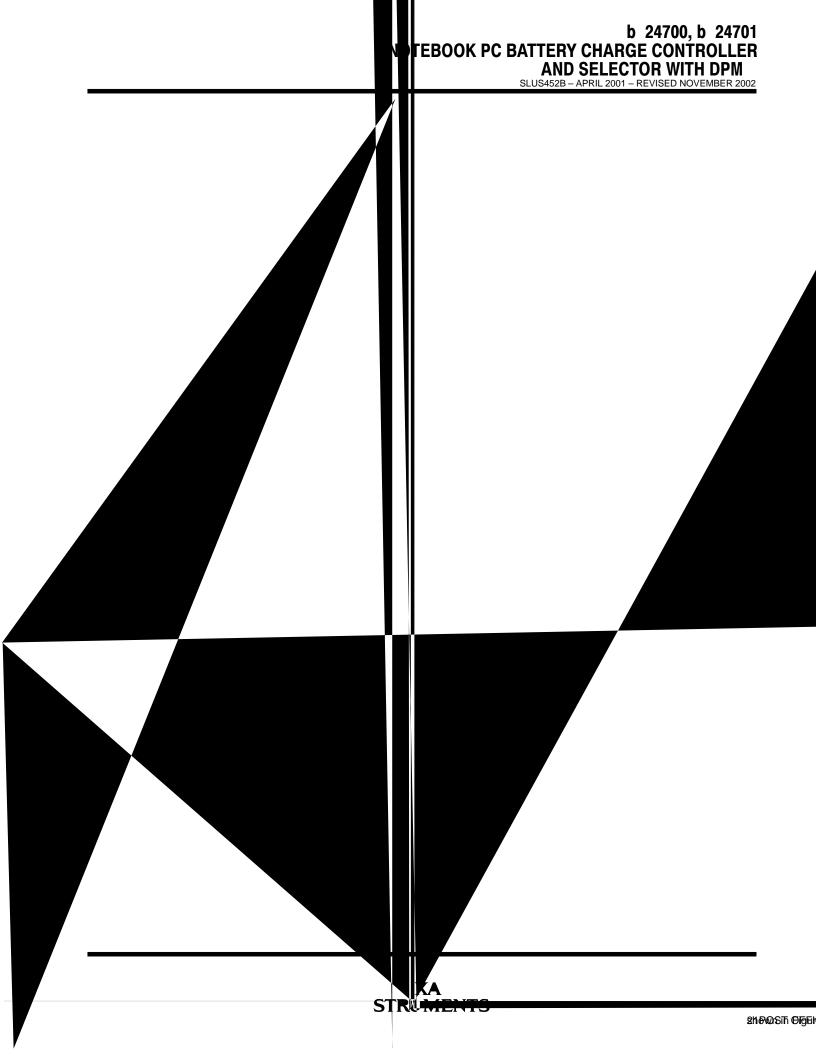
In addition, the higher ripple current results in an error in the sensed battery current particularly at lower charging currents. It is recommended that the ripple current not exceed 20% to 30% of full scale dc current.

$$L = \frac{\left(V_{IN} - V_{BAT}\right) \times V_{BAT}}{fs \times 0.2 \times I_{FS} \times V_{IN}}$$

Too large an inductor value results in the current waveform of Q1 and D1 in Figure 8 approximating a

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b 24700, b 24701 NOTEBOOK PC BATTERY CHARGE CONTROLLER

AND SELECTOR WITH DPM SLUS452B – APRIL 2001 – REVISED NOVEMBER 2002



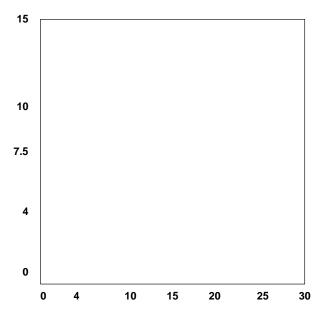
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APPLICATION INFORMATION

PWM selector switch gate drive

Because the external P-channel MOSFETs (as well as the internal MOSFETs) have a maximum gate-source voltage limitation of 20 V, the input voltage, VCC, cannot be used directly to drive the MOSFET gate under all input conditions. To provide safe MOSFET-gate-drive at input voltages of less than 20 V, an intermediate gate drive voltage rail was established (VSHP). As shown in Figure 11, VSHP has a stepped profile. For VCC voltages of less than 15 V, VSHP = 0 and the full VCC voltage is used to drive the MOSFET gate. At input voltages of greater than 15 V, VSHP steps to approximately one-half the VCC voltage. This ensures adequate enhancement voltage across all operating conditions.

The gate drive voltage, Vgs, vs VCC for the PWM, and ac selector P-channel MOSFETs are shown in Figure 11.



TYPICAL CHARACTERISTICS

ERROR AMPLIFIER REFERENCE vs JUNCTION TEMPERATURE 1.250 REF2 - Error Amplifier Reference -V 1.248 1.246 1.244 1.242 1.240 100 -40 -20 20 40 60 T_J – Junction Temperature – $^{\circ}$ C

Figure 12

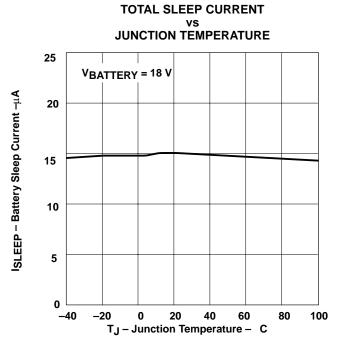


Figure 14

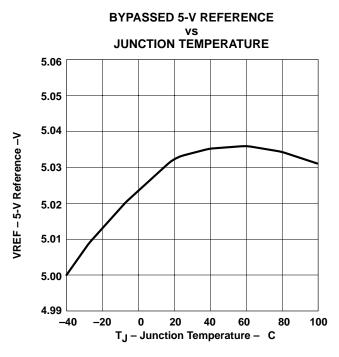


Figure 13

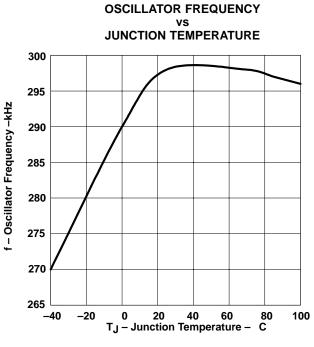


Figure 15







v.ti.com 21-Jan-2008

PACKAGING INFORMATION

Orderable Device	Status ⁽¹⁾	Package Type	Package Drawing	Pins Package Qty	Eco Plan (2)	Lead/Ball Finish	MSL Peak Temp ⁽³⁾
BQ24700PW	OBSOLETE	TSSOP	PW	24	TBD	Call TI	Call TI
BQ24700PWR	OBSOLETE	TSSOP	PW	24	TBD	Call TI	Call TI
BQ24700PWRG4	OBSOLETE	TSSOP	PW	24	TBD	Call TI	Call TI
BQ24701PW	OBSOLETE	TSSOP	PW	24	TBD	Call TI	Call TI
BQ24701PWG4	OBSOLETE	TSSOP	PW	24	TBD	Call TI	Call TI
BQ24701PWR	OBSOLETE	TSSOP	PW	24	TBD	Call TI	Call TI
BQ24701PWRG4	OBSOLETE	TSSOP	PW	24	TBD	Call TI	Call TI

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

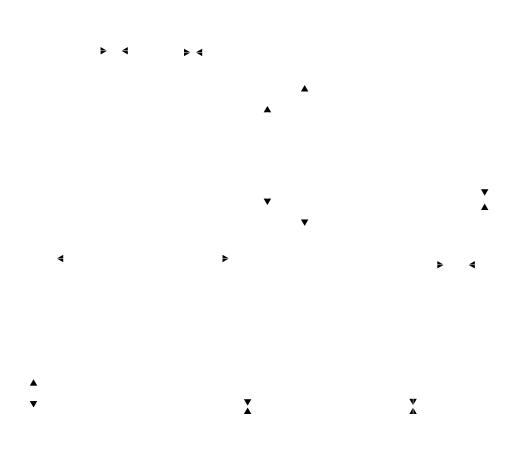
Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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